

MP-282

# Dynamic Modeling and Control of Multicopter Aerial Vehicles

## Chapter 5: Translational Motion, Euler Lagrange, and Summary

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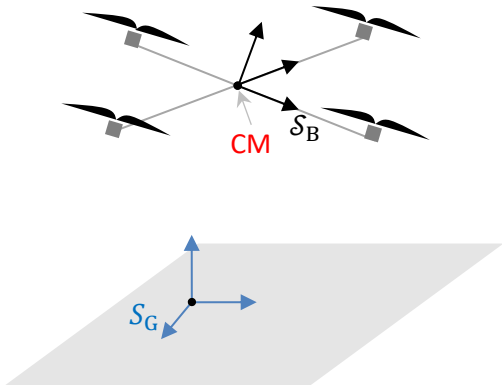
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## Coordinate Systems . . .

# Coordinate Systems

## Two Cartesian Coordinate Systems

In this section, we consider the **body CCS**  $\mathcal{S}_B \triangleq \{B; \hat{x}_B, \hat{y}_B, \hat{z}_B\}$  and the **ground CCS**  $\mathcal{S}_G \triangleq \{G; \hat{x}_G, \hat{y}_G, \hat{z}_G\}$ , where  $B \equiv \text{CM}$ .

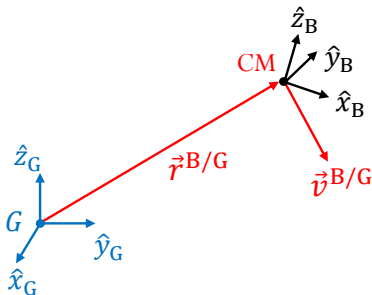


## Kinematic Equation . . .

# Kinematic Equation

## Scope

- $\vec{r}^{B/G}$ : position vector of  $\mathcal{S}_B$  w.r.t.  $\mathcal{S}_G$ .
- $\vec{v}^{B/G} \triangleq \frac{d}{dt} \vec{r}^{B/G}$ : velocity vector of  $\mathcal{S}_B$  w.r.t.  $\mathcal{S}_G$  as observed from  $\mathcal{S}_G$ .



The kinematics are represented by the time evolution of  $\vec{r}^{B/G}$  as a function of  $\vec{v}^{B/G}$ .

# Kinematic Equation

## Model

The translational kinematics of  $\mathcal{S}_B$  w.r.t.  $\mathcal{S}_G$  are modeled in  $\mathcal{S}_G$  by

$$\dot{\mathbf{r}}_G^{B/G} = \mathbf{v}_G^{B/G}$$

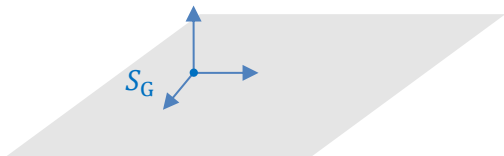
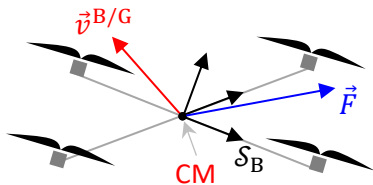
## Dynamic Equation . . .



# Dynamic Equation

## Scope

Denote the resulting external force by  $\vec{F}$ . The translational dynamics are represented by the time evolution of  $\vec{v}^{B/G}$  as a function of  $\vec{F}$ .



# Dynamic Equation

## Assumptions

Assume that

- 1  $\mathcal{S}_G$  is an inertial frame.
- 2  $\vec{F} = \vec{F}^c + \vec{F}^g + \vec{F}^d$ <sup>1</sup>.
- 3  $\vec{F}^c$ ,  $\vec{F}^g$ ,  $\vec{F}^d$  are modeled as in [Chapter 2](#).

## Newton's Law

The Second Newton's Law gives

$$\frac{d}{dt} \vec{v}^{B/G} = \frac{1}{m} \vec{F}$$

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<sup>1</sup>For simplicity, we are not considering specific forces, e.g., due to a balloon, a tether, or blading flapping. However, the extension should be smooth.

# Dynamic Equation

## Model

The translational dynamics of  $\mathcal{S}_B$  w.r.t.  $\mathcal{S}_G$  are modeled in  $\mathcal{S}_G$  by

$$\dot{\mathbf{v}}_G^{B/G} = \frac{1}{m} \left( \mathbf{D}^{B/G} \right)^T \mathbf{F}_B^c + \frac{1}{m} \mathbf{F}_G^g + \frac{1}{m} \mathbf{F}_G^d$$

where  $\mathbf{D}^{B/G} \equiv \mathbf{D}^{B/R}$ , which is known from [Chapter 4](#), and the models for  $\mathbf{F}_B^c$ ,  $\mathbf{F}_G^g$ , as well as  $\mathbf{F}_G^d$  are given in [Chapter 2](#).

## Euler-Lagrange Formulation ...

## Generalized Coordinates

Define the vector of **generalized coordinates**:

$$\mathbf{x} \triangleq \left[ \left( \mathbf{r}_G^{B/G} \right)^T \boldsymbol{\alpha}^T \right]^T$$

where  $\boldsymbol{\alpha} \triangleq [\phi \ \theta \ \psi]^T$  is the vector of **Euler angles** 123.

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<sup>2</sup>This section is based on reference [1], pp. 25–28.

# Euler-Lagrange Formulation

## Lagrangean

The Lagrangean of our six-DOF system is given by:

$$\mathcal{L} \triangleq K_t + K_r - P$$

where

- $K_t \triangleq \frac{m}{2} \left( \dot{\mathbf{r}}_G^{B/G} \right)^T \dot{\mathbf{r}}_G^{B/G}$  is the translational kinetic energy.
- $K_r \triangleq \frac{1}{2} \left( \boldsymbol{\Omega}_B^{B/R} \right)^T \mathbf{J}_B \boldsymbol{\Omega}_B^{B/R}$  is the rotational kinetic energy.
- $P \triangleq m g e_3^T \mathbf{r}_G^{B/G}$  is the potential energy.

# Euler-Lagrange Formulation

## Attitude Kinematic (Euler angles 123)

From [Chapter 4](#), we know that <sup>3</sup>

$$\boldsymbol{\Omega}_B^{B/R} = \mathcal{A}(\boldsymbol{\alpha})^{-1} \dot{\boldsymbol{\alpha}}$$

where

$$\mathcal{A}(\boldsymbol{\alpha})^{-1} = \begin{bmatrix} c\theta c\psi & s\psi & 0 \\ -c\theta s\psi & c\psi & 0 \\ s\theta & 0 & 1 \end{bmatrix}$$

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<sup>3</sup>A similar derivation can be done for any attitude representation seen in [Chapter 4](#).

# Euler-Lagrange Formulation

## Rotational Kinetic Energy

Using the above equation, it can be rewritten in the form

$$K_r = \frac{1}{2} \dot{\alpha}^T \mathbb{J} \dot{\alpha}$$

where

$$\mathbb{J} \triangleq \mathcal{A}(\alpha)^{-T} \mathbf{J}_B \mathcal{A}(\alpha)^{-1}$$



# Euler-Lagrange Formulation

## Euler-Lagrange Equation

The Euler-Lagrange equation for the system under consideration is

$$\frac{d}{dt} \left( \frac{\partial \mathcal{L}}{\partial \dot{\mathbf{x}}} \right) - \frac{\partial \mathcal{L}}{\partial \mathbf{x}} = \begin{bmatrix} \mathbf{F}_G \\ \mathbf{T}_B \end{bmatrix}$$

where  $\mathbf{F}_G$  is the  $\mathcal{S}_G$  representation of the resulting force and  $\mathbf{T}_B$  is the  $\mathcal{S}_B$  representation of the resulting torque.

### Remark:

Since  $\mathcal{L}$  does not contain terms involving both  $\mathbf{r}_G^{B/G}$  and  $\dot{\boldsymbol{\alpha}}$  together, we can separate the above equation into two parts: one for the translation and the other one for the rotation.

# Euler-Lagrange Formulation

## Translation

Define the translation Lagrangean as  $\mathcal{L}_t \triangleq K_t - P$ . Therefore, according to the Euler-Lagrange formulation, the translational equation of motion is obtained from

$$\frac{d}{dt} \left( \frac{\partial \mathcal{L}_t}{\partial \dot{\mathbf{r}}_G^{B/G}} \right) - \frac{\partial \mathcal{L}_t}{\partial \mathbf{r}_G^{B/G}} = \mathbf{F}_G$$

as

$$m \ddot{\mathbf{r}}_G^{B/G} = \mathbf{F}_G - mg \mathbf{e}_3$$

which coincides with the Newton's Second Law.

# Euler-Lagrange Formulation

## Rotation

Define the rotation Lagrangean as  $\mathcal{L}_r \triangleq K_r$ . According to the Euler-Lagrange formulation, the rotational equation of motion is obtained from

$$\frac{d}{dt} \left( \frac{\partial \mathcal{L}_r}{\partial \dot{\alpha}} \right) - \frac{\partial \mathcal{L}_r}{\partial \alpha} = \mathbf{T}_B$$

as

$$\mathbb{J} \ddot{\alpha} + C(\alpha, \dot{\alpha}) \dot{\alpha} = \mathbf{T}_B$$

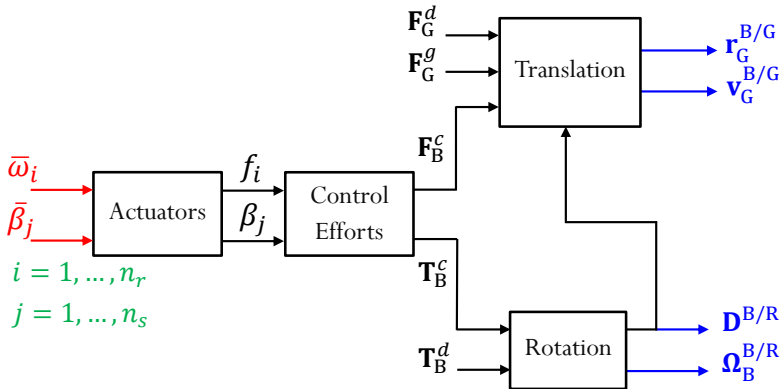
where

$$C(\alpha, \dot{\alpha}) \triangleq -\frac{1}{2} \dot{\alpha}^T \left( \mathbf{A}(\alpha)^{-T} \mathbf{J}_B \frac{\partial}{\partial \alpha} \left( \mathbf{A}(\alpha)^{-1} \right) + \frac{\partial}{\partial \alpha} \left( \mathbf{A}(\alpha)^{-T} \right) \mathbf{J}_B \mathbf{A}(\alpha) \right)$$

Summary . . .

# Summary



## Overall MAV Modeling <sup>4</sup>



<sup>4</sup>This block diagram does not consider a balloon neither a tether.

References . . .

# References

-  [1] Goldstein, H. **Classical Mechanics**. Addison-Wesley, 1950.
-  [2] Carrillo, L.R.G., Lopez, A.E.D., Lozano, R., Pegard, C. **A Quad Rotorcraft Control - Vision-Based Hovering and Navigation**. Springer, 2013.

Thanks!