

MP-208

Optimal Filtering with Aerospace Applications
**Chapter 10: Navigation Using a Visual Fiducial System
and Inertial Measurements**

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Contents

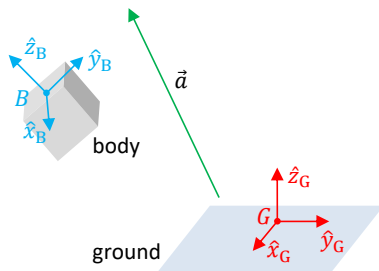
- 1 Notation and Preliminary Definitions
- 2 Kinematic Equations
- 3 Sensor Modeling
- 4 Problem Statement
- 5 Problem Solution

Notation and preliminaries . . .

Notation and Preliminary Definitions

Geometric Vectors and Cartesian Coordinate Systems

- \vec{a} : geometric (or physical) vector
- \hat{a} : unit geometric (physical) vector
- $\mathcal{S}_B \triangleq \{B; \hat{x}_B, \hat{y}_B, \hat{z}_B\}$: body Cartesian coordinate system (CCS)
- $\mathcal{S}_G \triangleq \{G; \hat{x}_G, \hat{y}_G, \hat{z}_G\}$: ground CCS



Notation and Preliminary Definitions

Algebraic Vectors and Attitude Matrices

- \mathbf{a}_B : representation of \vec{a} in \mathcal{S}_B (algebraic vector); $\mathbf{a}_B \in \mathbb{R}^3$
- \mathbf{a}_G : representation of \vec{a} in \mathcal{S}_G (algebraic vector); $\mathbf{a}_G \in \mathbb{R}^3$
- $\mathbf{D}^{B/G}$: attitude matrix of \mathcal{S}_B w.r.t. \mathcal{S}_G ; $\mathbf{D}^{B/G} \in \text{SO}(3)$ ¹

We can convert representations of a given geometric vector as below:

$$\mathbf{a}_B = \mathbf{D}^{B/G} \mathbf{a}_G$$

From this and the definition of $\text{SO}(3)$, we see that

$$\left(\mathbf{D}^{B/G}\right)^{-1} = \left(\mathbf{D}^{B/G}\right)^T = \mathbf{D}^{G/B}$$

¹ $\text{SO}(3) \triangleq \{\mathbf{D} \in \mathbb{R}^{3 \times 3} : \mathbf{D}\mathbf{D}^T = \mathbf{I}_3\}$ is the special orthogonal group.

Kinematic Equations

Euler Angles

Consider the elementary rotation matrices (about axis 1,2, and 3, resp.):

$$\mathbf{D}_1(\varrho) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & c\varrho & s\varrho \\ 0 & -s\varrho & c\varrho \end{bmatrix} \quad \mathbf{D}_2(\varrho) = \begin{bmatrix} c\varrho & 0 & -s\varrho \\ 0 & 1 & 0 \\ s\varrho & 0 & c\varrho \end{bmatrix}$$
$$\mathbf{D}_3(\varrho) = \begin{bmatrix} c\varrho & s\varrho & 0 \\ -s\varrho & c\varrho & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

For example, considering a 1-2-3 sequence of rotations of angles denoted by ϕ , θ , and ψ , respectively, the relationship between these (Euler) angles and the attitude matrix is

$$\mathbf{D}^{B/G} = \mathbf{D}_3(\psi)\mathbf{D}_2(\theta)\mathbf{D}_1(\phi)$$

Kinematic Equations

Attitude Kinematics

We can show that the **attitude kinematics** can be described in Euler angles 1-2-3 by

$$\dot{\boldsymbol{\alpha}}^{\text{B/G}} = \mathcal{A} \left(\boldsymbol{\alpha}^{\text{B/G}} \right) \boldsymbol{\omega}_{\text{B}}^{\text{B/R}} \quad (1)$$

where $\boldsymbol{\alpha}^{\text{B/G}} \triangleq [\phi \ \theta \ \psi]^{\text{T}}$, $\boldsymbol{\omega}_{\text{B}}^{\text{B/R}} \in \mathbb{R}^3$ is the \mathcal{S}_{B} representation of the angular velocity of \mathcal{S}_{B} w.r.t. \mathcal{S}_{G} , and

$$\mathcal{A} \left(\boldsymbol{\alpha}^{\text{B/G}} \right) \triangleq \begin{bmatrix} c\psi/c\theta & -s\psi/c\theta & 0 \\ s\psi & c\psi & 0 \\ -c\psi s\theta/c\theta & s\psi s\theta/c\theta & 1 \end{bmatrix}$$

Kinematic Equations

Position Kinematics

They are modeled by²

$$\frac{d}{dt_G} \vec{r}^{B/G} = \vec{v}^{B/G},$$

which can be represented in \mathcal{S}_G to give

$$\dot{\mathbf{r}}_G^{B/G} = \mathbf{v}_G^{B/G} \quad (2)$$

²The subindex G in the time derivative is to say that it is taken with respect to an observer on \mathcal{S}_G .

Sensor Modeling

Rate-Gyro:

Its measure $\check{\omega}_B^{B/G} \in \mathbb{R}^3$ is modeled by

$$\check{\omega}_B^{B/G} = \omega_B^{B/G} + \beta_B^g + \mathbf{w}_B^g \quad (3)$$

where $\mathbf{w}_B^g \in \mathbb{R}^3$ is a zero-mean random noise with covariance \mathbf{Q}^g (for simplicity, it is assumed constant and known) and $\beta_B^g \in \mathbb{R}^3$ is a bias described by the following Wiener process:

$$\dot{\beta}_B^g = \mathbf{w}_B^{\beta_g} \quad (4)$$

where $\mathbf{w}_B^{\beta_g}$ is a zero-mean random noise with covariance \mathbf{Q}^{β_g} (it is also assumed constant and known).

Sensor Modeling

Accelerometer:

Its measure $\check{\mathbf{a}}_B^{B/G} \in \mathbb{R}^3$ is modeled by

$$\check{\mathbf{a}}_B^{B/G} = \mathbf{D}^{B/G} \left(\dot{\mathbf{v}}_G^{B/G} - \mathbf{g}_G \right) + \boldsymbol{\beta}_B^a + \mathbf{w}_B^a \quad (5)$$

where $\mathbf{g}_G \triangleq -g\mathbf{e}_3$ is the gravity acceleration vector, $\mathbf{w}_B^a \in \mathbb{R}^3$ is a zero-mean random noise with covariance \mathbf{Q}^a (for simplicity, it is assumed constant and known), and $\boldsymbol{\beta}_B^a \in \mathbb{R}^3$ is a bias described by the following Wiener process:

$$\dot{\boldsymbol{\beta}}_B^a = \mathbf{w}_B^{\beta_a} \quad (6)$$

where $\mathbf{w}_B^{\beta_a}$ is a zero-mean random noise with covariance \mathbf{Q}^{β_a} (it is also assumed constant and known).

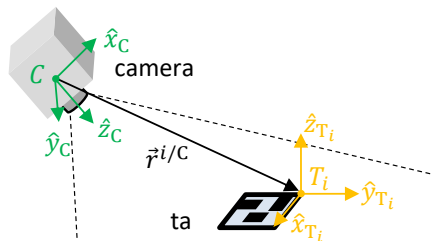
Sensor Modeling

Visual Fiducial System:

It could be the AprilTag system, for example. Its algorithm provides indirect measures of position $\vec{r}^{i/C}$ and attitude $\mathbf{D}^{i/C}$ of the tag w.r.t. \mathcal{S}_C . We consider just the first and assume that its measure is described by

$$\check{\mathbf{r}}_C^{i/C} = \mathbf{r}_C^{i/C} + \mathbf{n}_C^i \quad (7)$$

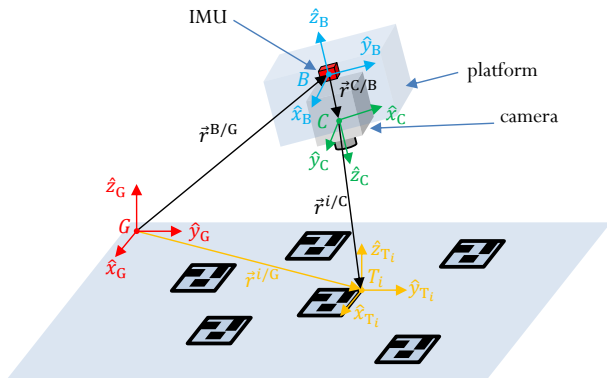
where $\mathbf{n}_C^i \in \mathbb{R}^3$ is a zero-mean noise with covariance \mathbf{R} (which, for simplicity, is assumed known and constant).



Problem Statement

Scenario

- The platform is a 6DOF box with a downward-facing camera and an inertial measurement unit (IMU).
- The ground has many mapped fiducial markers.

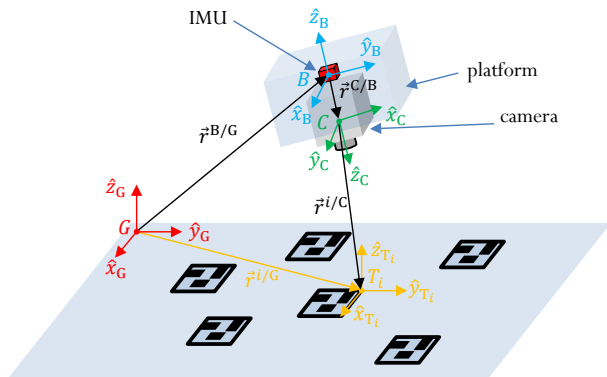


Problem Statement

Problem

It is to recursively estimate $\mathbf{r}_G^{B/G}$, $\mathbf{v}_G^{B/G}$, $\boldsymbol{\alpha}^{B/G}$, $\boldsymbol{\beta}_B^g$, and $\boldsymbol{\beta}_B^a$ using:

- the models (1)–(7) and
- the measurements $\hat{\mathbf{a}}_B^{B/G}$, $\hat{\boldsymbol{\omega}}_B^{B/G}$, and $\hat{\mathbf{r}}_C^{i/C}$.



Problem Solution

State Equation

The models (1)–(6) can be put together in the following state equation:

$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}, \mathbf{u}) + \mathbf{G}(\mathbf{x}) \mathbf{w}, \quad (8)$$

where

$$\mathbf{x} \triangleq \left[\left(\mathbf{r}_G^{B/G} \right)^T \quad \left(\mathbf{v}_G^{B/G} \right)^T \quad \left(\boldsymbol{\alpha}^{B/G} \right)^T \quad \left(\boldsymbol{\beta}_B^a \right)^T \quad \left(\boldsymbol{\beta}_B^g \right)^T \right]^T \in \mathbb{R}^{15}$$

$$\mathbf{u} \triangleq \left[\left(\check{\mathbf{a}}_B^{B/G} \right)^T \quad \left(\check{\boldsymbol{\omega}}_B^{B/G} \right)^T \right]^T \in \mathbb{R}^6$$

$$\mathbf{w} \triangleq \left[\left(\mathbf{w}_B^a \right)^T \quad \left(\mathbf{w}_B^g \right)^T \quad \left(\mathbf{w}^{\beta_a} \right)^T \quad \left(\mathbf{w}^{\beta_g} \right)^T \right]^T \in \mathbb{R}^{12}$$

Problem Solution

State Equation (Cont.)

$$\mathbf{f}(\mathbf{x}, \mathbf{u}) \triangleq \begin{bmatrix} \mathbf{D}^T \left(\boldsymbol{\alpha}^{B/G} \right) \left(\overset{\mathbf{v}_G^{B/G}}{\check{\mathbf{a}}_B^{B/G}} - \boldsymbol{\beta}_B^a \right) + \mathbf{g}_G \\ \mathcal{A} \left(\boldsymbol{\alpha}^{B/G} \right) \left(\check{\boldsymbol{\omega}}_B^{B/G} - \boldsymbol{\beta}_B^g \right) \\ \mathbf{0}_{3 \times 1} \\ \mathbf{0}_{3 \times 1} \end{bmatrix} \in \mathbb{R}^{15}$$
$$\mathbf{G}(\mathbf{x}) \triangleq \begin{bmatrix} \mathbf{0}_{3 \times 3} & \mathbf{0}_{3 \times 3} & \mathbf{0}_{3 \times 3} & \mathbf{0}_{3 \times 3} \\ -\mathbf{D}^T \left(\boldsymbol{\alpha}^{B/G} \right) & \mathbf{0}_{3 \times 3} & \mathbf{0}_{3 \times 3} & \mathbf{0}_{3 \times 3} \\ \mathbf{0}_{3 \times 3} & -\mathcal{A} \left(\boldsymbol{\alpha}^{B/G} \right) & \mathbf{0}_{3 \times 3} & \mathbf{0}_{3 \times 3} \\ \mathbf{0}_{3 \times 3} & \mathbf{0}_{3 \times 3} & \mathbf{I}_3 & \mathbf{0}_{3 \times 3} \\ \mathbf{0}_{3 \times 3} & \mathbf{0}_{3 \times 3} & \mathbf{0}_{3 \times 3} & \mathbf{I}_3 \end{bmatrix} \in \mathbb{R}^{15 \times 12}$$

Problem Solution

State Equation (Cont.)

$$\mathbf{D}(\boldsymbol{\alpha}^{B/G}) = \mathbf{D}_3(\psi)\mathbf{D}_2(\theta)\mathbf{D}_1(\phi) \in \text{SO}(3)$$

and

$$\phi \triangleq \mathbf{e}_1^T \boldsymbol{\alpha}^{B/G}$$

$$\theta \triangleq \mathbf{e}_2^T \boldsymbol{\alpha}^{B/G}$$

$$\psi \triangleq \mathbf{e}_3^T \boldsymbol{\alpha}^{B/G}$$

Problem Solution

Measurement Equations

Using the problem geometry (see the scenario on slide 11) and equation (7), the measurement equations can be derived as:

$$\mathbf{y}^i = \mathbf{h}^i(\mathbf{x}) + \mathbf{n}^i, \quad i = 1, \dots, q \quad (9)$$

where $q \in \mathbb{Z}_+$ is the number of visible markers, $\mathbf{n}^i \equiv \mathbf{n}_C^i$, $\mathbf{y}^i \triangleq \check{\mathbf{r}}_C^{i/C}$ and

$$\mathbf{h}^i(\mathbf{x}) \triangleq \mathbf{D}^{C/B} \left(\mathbf{D} \left(\boldsymbol{\alpha}^{B/G} \right) \left(\mathbf{r}_G^{i/G} - \mathbf{r}_G^{B/G} \right) - \mathbf{r}_B^{C/B} \right)$$

Now we are ready for the computational exercise!



Santos, D. A. **Notas de aula de MP-282 – Dynamic Modeling and Control of Multicopters**. ITA, 2018. [Chapter 4]