

MP-208

# Optimal Filtering with Aerospace Applications

## Chapter 9: Attitude Determination for Drones

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Introduction...

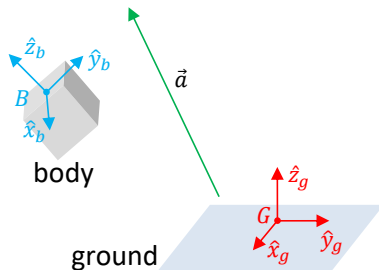
## Scope of the Chapter

- This chapter is concerned with a **three-dimensional attitude determination** scheme for **drones**.
- The adopted attitude/navigation sensors are **rate gyros**, **accelerometers**, and **magnetometers**, all three-axial.
- **This presentation only formulates the problem**. The problem solution will be presented by the students, using **CDEKF**, **CDUKF**, and **CDE<sub>n</sub>KF** as the final evaluation of the course, according to a specific assignment.

# Introduction

## Notation

- $\vec{a}$ : geometric (or physical) vector.
- $\hat{a}$ : geometric (or physical) vector.
- $B, G$ : tridimensional points.
- $S_b \triangleq \{B; \hat{x}_b, \hat{y}_b, \hat{z}_b\}$ : body Cartesian coordinate system (CCS).
- $S_g \triangleq \{G; \hat{x}_g, \hat{y}_g, \hat{z}_g\}$ : ground CCS.



# Introduction

## Notation (cont.)

- $\mathbf{a}_b \in \mathbb{R}^3$ : representation of  $\vec{a}$  in  $\mathcal{S}_b$  (algebraic vector).
- $\mathbf{a}_g \in \mathbb{R}^3$ : representation of  $\vec{a}$  in  $\mathcal{S}_g$  (algebraic vector).
- $\mathbf{D}^{b/g} \in \text{SO}(3)$ : attitude matrix of  $\mathcal{S}_b$  w.r.t.  $\mathcal{S}_g$ .<sup>1</sup>

We can convert representations of a given geometric vector as follows:

$$\mathbf{a}_b = \mathbf{D}^{b/g} \mathbf{a}_g$$

From this and the definition of  $\text{SO}(3)$ , we see that

$$\left(\mathbf{D}^{b/g}\right)^{-1} = \left(\mathbf{D}^{b/g}\right)^{\text{T}} = \mathbf{D}^{g/b}$$

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<sup>1</sup> $\text{SO}(3) \triangleq \{\mathbf{D} \in \mathbb{R}^{3 \times 3} : \mathbf{D}\mathbf{D}^{\text{T}} = \mathbf{I}_3\}$  is the special orthogonal group.

# Introduction

## Notation (*cont.*)

Consider the elementary rotation matrices (about axes 1, 2, and 3, resp.):

$$\mathbf{D}_1(\varrho) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & c\varrho & s\varrho \\ 0 & -s\varrho & c\varrho \end{bmatrix} \quad \mathbf{D}_2(\varrho) = \begin{bmatrix} c\varrho & 0 & -s\varrho \\ 0 & 1 & 0 \\ s\varrho & 0 & c\varrho \end{bmatrix}$$
$$\mathbf{D}_3(\varrho) = \begin{bmatrix} c\varrho & s\varrho & 0 \\ -s\varrho & c\varrho & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

For example, considering a 1-2-3 sequence of rotations of angles denoted by  $\phi$ ,  $\theta$ , and  $\psi$ , respectively, the relationship between these (Euler) angles and the attitude matrix is

$$\mathbf{D}^{b/g} = \mathbf{D}_3(\psi)\mathbf{D}_2(\theta)\mathbf{D}_1(\phi)$$

Kinematic equations. . .



# Kinematic Equations

## Attitude Kinematics in Euler Angles 1-2-3

We can show that the **attitude kinematics** can be described in Euler angles in the 1-2-3 sequence by

$$\dot{\alpha}^{b/g} = \mathbf{A} \left( \alpha^{b/g} \right) \omega_b^{b/g} \quad (1)$$

where  $\alpha^{b/g} \triangleq (\phi, \theta, \psi)$ ,  $\omega_b^{b/g} \in \mathbb{R}^3$  is the  $\mathcal{S}_b$  representation of the angular velocity of  $\mathcal{S}_b$  w.r.t.  $\mathcal{S}_g$ , and

$$\mathbf{A} \left( \alpha^{b/g} \right) \triangleq \begin{bmatrix} c\psi/c\theta & -s\psi/c\theta & 0 \\ s\psi & c\psi & 0 \\ -c\psi s\theta/c\theta & s\psi s\theta/c\theta & 1 \end{bmatrix}$$

Sensor modeling. . .

## Rate Gyro

Its measure  $\check{\omega}_b \in \mathbb{R}^3$  can be modeled by

$$\check{\omega}_b = \omega_b^{b/g} + \beta_b^{gy} + \mathbf{w}_b^{gy} \quad (2)$$

where  $\mathbf{w}_b^{gy} \in \mathbb{R}^3$  is a zero-mean white Gaussian noise with covariance  $\mathbf{Q}^{gy}$ , which, for simplicity, is assumed to be constant and known, and  $\beta_b^{gy} \in \mathbb{R}^3$  is a drifting bias described by the following Wiener process:

$$\dot{\beta}_b^{gy} = \mathbf{w}_b^{d,gy} \quad (3)$$

where  $\mathbf{w}_b^{d,gy}$  is assumed to be a zero-mean white Gaussian noise with known covariance  $\mathbf{Q}^{d,gy}$ .

## Accelerometer

Its measure  $\check{\mathbf{a}}_b \in \mathbb{R}^3$  can be modeled by

$$\check{\mathbf{a}}_b = \mathbf{D}^{b/g} \left( \dot{\mathbf{v}}_g^{b/g} - \mathbf{g}_g \right) + \mathbf{w}_b^{ac} \quad (4)$$

where  $\mathbf{g}_g \triangleq -g\mathbf{e}_3$  is the gravity acceleration vector, and  $\mathbf{w}_b^{ac} \in \mathbb{R}^3$  is assumed to be a zero-mean white Gaussian noise with known covariance  $\mathbf{Q}^{ac}$ .

**Assume** that  $\dot{\mathbf{v}}_g^{b/g} = 0$  along all the flight, which is a reasonable simplification as one could verify by an MAV flight control simulator<sup>2</sup>.

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<sup>2</sup>IMAV-M is available in <https://github.com/daviasantos/IMAV-M>.

## Magnetometer

Its measure  $\check{\mathbf{m}}_b \in \mathbb{R}^3$  can be modeled by

$$\check{\mathbf{m}}_b = \mathbf{D}^{b/g} \mathbf{m}_g + \mathbf{w}_b^{mg} \quad (5)$$

where  $\mathbf{m}_g \in \mathbb{R}^3$  is the  $\mathcal{S}_g$  representation of the local magnetic field and  $\mathbf{w}_b^{mg} \in \mathbb{R}^3$  is assumed to be a zero-mean white Gaussian noise with known covariance  $\mathbf{Q}^{mg}$ .

**Assume** that  $\mathbf{m}_g$  keeps constant along the drone flight.

Problem statement. . .

# Problem Statement

## Problem

The problem is to estimate  $\alpha^{b/g}$  and  $\beta_b^{gy}$ , by a recursive approximately optimal filter, using:

- the models (1)–(5) and
- the measurements  $\check{\mathbf{a}}_b$ ,  $\check{\omega}_b$ , and  $\check{\mathbf{m}}_b$ .

Problem solution...



# Problem Solution

## State Equation

The models (1)–(3) can be put together in the following state equation:

$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}, \mathbf{u}) + \mathbf{G}(\mathbf{x}) \mathbf{w}, \quad (6)$$

where

$$\mathbf{x} \triangleq \left[ \left( \boldsymbol{\alpha}^{b/g} \right)^T \left( \boldsymbol{\beta}_b^{gy} \right)^T \right]^T \in \mathbb{R}^6$$

$$\mathbf{u} \triangleq \check{\boldsymbol{\omega}}_b \in \mathbb{R}^3$$

$$\mathbf{w} \triangleq \left[ \left( \mathbf{w}_b^{gy} \right)^T \left( \mathbf{w}_b^{d,gy} \right)^T \right]^T \in \mathbb{R}^6$$

# Problem Solution

## State Equation (*cont.*)

$$\mathbf{f}(\mathbf{x}, \mathbf{u}) \triangleq \begin{bmatrix} \mathbf{A}(\boldsymbol{\alpha}^{b/g}) \left( \check{\boldsymbol{\omega}}_b^{b/g} - \boldsymbol{\beta}_b^{gy} \right) \\ \mathbf{0}_{3 \times 1} \end{bmatrix} \in \mathbb{R}^6$$

$$\mathbf{G}(\mathbf{x}) \triangleq \begin{bmatrix} -\mathbf{A}(\boldsymbol{\alpha}^{b/g}) & \mathbf{0}_{3 \times 3} \\ \mathbf{0}_{3 \times 3} & \mathbf{I}_3 \end{bmatrix} \in \mathbb{R}^{6 \times 6}$$

# Problem Solution

## Measurement Equation

Equations (4) and (5) can be put together into the following discrete-time measurement equation:

$$\mathbf{y}_k = \mathbf{h}(\mathbf{x}_k) + \mathbf{v}_k \quad (7)$$

where (for simplicity, we omit the time  $t_k$  from the time-varying quantities)

$$\mathbf{y}_k \triangleq \begin{bmatrix} \check{\mathbf{a}}_b/g \\ \check{\mathbf{m}}_b/\|\mathbf{m}_g\| \end{bmatrix}, \quad \mathbf{h}(\mathbf{x}_k) \triangleq \begin{bmatrix} \mathbf{D}(\boldsymbol{\alpha}^{b/g}) \mathbf{e}_3 \\ \mathbf{D}(\boldsymbol{\alpha}^{b/g}) \mathbf{n} \end{bmatrix}, \quad \mathbf{v}_k \triangleq \begin{bmatrix} \mathbf{w}_b^{ac}/g \\ \mathbf{w}_b^{mg}/\|\mathbf{m}_g\| \end{bmatrix}$$

$$\mathbf{D}(\boldsymbol{\alpha}^{b/g}) \triangleq \mathbf{D}_3(\psi)\mathbf{D}_2(\theta)\mathbf{D}_1(\phi), \quad \mathbf{n} \triangleq \mathbf{m}_g/\|\mathbf{m}_g\|$$

with  $\phi \triangleq \mathbf{e}_1^T \boldsymbol{\alpha}^{b/g}$ ,  $\theta \triangleq \mathbf{e}_2^T \boldsymbol{\alpha}^{b/g}$ ,  $\psi \triangleq \mathbf{e}_3^T \boldsymbol{\alpha}^{b/g}$ , and  $\mathbf{e}_i$ ,  $\forall i$ , denoting the standard unit vectors.

References. . .



Santos, D. A. **Dynamic Modeling and Control of Multicopters. Chapter 4.** Available in [www.professordavisantos.com](http://www.professordavisantos.com). ITA, 2020.